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Lattice Boltzmann Approach

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Computer Simulations of Systems with Hydrodynamic Interactions: The Coupled Molecular Dynamics – Lattice Boltzmann Approach

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In soft-matter systems where Brownian constituents are immersed in a solvent, both thermal fluctuations and hydrodynamic interactions are important. The article outlines a general scheme to simulate such systems by coupling Molecular Dynamics for the Brownian particles to a lattice Boltzmann algorithm for the solvent. As an application, the computer simulation of colloidal electrophoresis is briefly discussed.

1 Introduction

Remark: The present contribution intends to just give a very brief overview over the subject matter. The author has recently, together with A. J. C. Ladd, written a 76-page review article¹, to which the interested reader is referred. Detailed explanations and derivations, as well as an extended reference list, can be found there. —

Many soft-matter systems are comprised of Brownian particles immersed in a solvent. Prototypical examples are colloidal dispersions and polymer solutions, where the latter, in contrast to the former, are characterized by non-trivial internal degrees of freedom (here: the many possible conformations of the macromolecule). Fundamental for these systems is the separation of length and time scales between “large and slow” Brownian particles, and “small and fast” solvent particles. “Mesoscopic” simulations focus on the range of length and time scales which are, on the one hand, too small to allow a description just in terms of continuum mechanics of the overall system, but, on the other hand, large enough to allow the replacement of the solvent by a hydrodynamic continuum. This latter approximation is much less severe than one would assume at first glance; detailed Molecular Dynamics simulations have shown that hydrodynamics works as soon as the length scale exceeds a few particle diameters, and the time scale a few collision times.

To simulate such systems consistently, one has to take into account that the length and time scales are so small that thermal fluctuations cannot be neglected. The “Boltzmann number” Bo (a term invented by us) is a useful parameter for quantifying how important fluctuations are. Given a certain spatial resolution b (for example, the lattice spacing of a grid which is used to simulate the fluid dynamics), we may ask ourselves how many solvent particles N_p correspond to the scale b . On average, this is given by $N_p = \rho b^3 / m_p$, where ρ is the mass density and m_p the mass of a solvent particle (and we assume a three-

dimensional system). The relative importance of fluctuations is then given by

$$Bo = N_p^{-1/2} = \left(\frac{m_p}{\rho b^3} \right)^{1/2}. \quad (1)$$

It should be noted that for an ideal gas, where the occupation statistics is Poissonian, Bo is just the relative statistical inaccuracy of the random variable N_p . In soft-matter systems, b is usually small enough such that Bo is no longer negligible.

Furthermore, *hydrodynamic interactions* must be modeled. In essence, this term refers to dynamic correlations between the Brownian particles, mediated by fast momentum transport through the solvent. The separation of time scales can be quantified in terms of the so-called Schmidt number

$$Sc = \frac{\eta_{kin}}{D}, \quad (2)$$

where $\eta_{kin} = \eta/\rho$ is the kinematic viscosity (ratio of dynamic shear viscosity η and mass density ρ) of the fluid, measuring how quickly momentum propagates diffusively through the solvent, and D is the diffusion constant of the particles. Typically, in a dense fluid $Sc \sim 10^2 \dots 10^3$ for the solvent particles, while for large Brownian particles Sc is even much larger. Finally, we may also often assume that the solvent dynamics is in the creeping-flow regime, i. e. that the Reynolds number

$$Re = \frac{ul}{\eta_{kin}}, \quad (3)$$

where u denotes the velocity of the flow and l its typical size, is small. This is certainly true as long as the system is not driven strongly out of thermal equilibrium.

These considerations lead to the natural (but, in our opinion, not always correct) conclusion that the method of choice to simulate such systems is Brownian Dynamics². Here the Brownian particles are displaced under the influence of particle-particle forces, hydrodynamic drag forces (calculated from the particle positions), and stochastic forces representing the thermal noise. However, the technical problems to do this efficiently for a large number N of Brownian particles are substantial. The calculation of the drag forces involves the evaluation of the hydrodynamic Green's function, which depends on the boundary conditions, and has an intrinsically long-range nature (such that all particles interact with each other). Furthermore, these drag terms also determine the correlations in the stochastic displacements, such that the generation of the stochastic terms involves the calculation of the matrix square root of a $3N \times 3N$ matrix. Recently, there has been substantial progress in the development of fast algorithms³; however, currently there are only few groups who master these advanced and complicated techniques. Apart from this, the applicability is somewhat limited, since the Green's function must be re-calculated for each new boundary condition, and its validity is questionable if the system is put under strong nonequilibrium conditions like, e. g., a turbulent flow — it should be noted that the Green's function is calculated for low- Re hydrodynamics.

Therefore, many soft-matter researchers have rather chosen the alternative approach, which is to simulate the system including the solvent degrees of freedom, with explicit momentum transport. The advantage of this is a simple algorithm, which scales linearly with the number of Brownian particles, and is easily parallelizable, due to its locality. The disadvantage, however, is that one needs to simulate many more degrees of freedom than

those in which one is genuinely interested — *and* to do this on the short inertial time scales in which one is not interested either. It is clear that such an approach involves essentially Molecular Dynamics (MD) for the Brownian particles.

Many ways are possible how to simulate the solvent degrees of freedom, and how to couple them to the MD part. It is just the universality of hydrodynamics that allows us to invent many models which all will produce the correct physics. The requirements are rather weak — the solvent model has to just be compatible with Navier–Stokes hydrodynamics on the macroscopic scale. Particle methods include Dissipative Particle Dynamics (DPD) and Multi-Particle Collision Dynamics (MPCD)⁴, while lattice methods involve the direct solution of the Navier–Stokes equation on a lattice, or lattice Boltzmann (LB). The latter is a method with which we have made quite good experience, both in terms of efficiency and versatility. The efficiency comes from the inherent ease of memory management for a lattice model, combined with ease of parallelization, which comes from the high degree of locality: Essentially an LB algorithm just shifts populations on a lattice, combined with collisions, which however only happen locally on a single lattice site. The coupling to the Brownian particles (simulated via MD) can either be done via boundary conditions, or via an interpolation function that introduces a *dissipative* coupling between particles and fluid. In this article, we will focus on the latter method.

2 Coupling Scheme

As long as we view LB as just a solver for the Navier–Stokes equation, we may write down the equations of motion for the coupled system as follows:

$$\frac{d}{dt}\vec{r}_i = \frac{1}{m_i}\vec{p}_i, \quad (4)$$

$$\frac{d}{dt}\vec{p}_i = \vec{F}_i^c + \vec{F}_i^d + \vec{F}_i^f, \quad (5)$$

$$\partial_t \rho + \partial_\alpha j_\alpha = 0, \quad (6)$$

$$\partial_t j_\alpha + \partial_\beta \pi_{\alpha\beta}^E = \partial_\beta \eta_{\alpha\beta\gamma\delta} \partial_\gamma u_\delta + f_\alpha^h + \partial_\beta \sigma_{\alpha\beta}^f. \quad (7)$$

Here, \vec{r}_i , \vec{p}_i and m_i are the positions, momenta, and masses of the Brownian particles, respectively. The forces \vec{F}_i acting on the particles are conservative (*c*, i. e. coming from the interparticle potential), dissipative (*d*), and fluctuating (*f*). The equations of motion for the fluid have been written in tensor notation, where Greek indexes denote Cartesian components, and the Einstein summation convention is used. The first equation describes mass conservation; the mass flux $\rho\vec{u}$, where \vec{u} is the flow velocity, is identical to the momentum density \vec{j} . The last equation describes the time evolution of the fluid momentum density. In the absence of particles, the fluid momentum is conserved. This part is described via the stress tensor, which in turn is decomposed into the conservative Euler stress $\pi_{\alpha\beta}^E$, the dissipative stress $\eta_{\alpha\beta\gamma\delta} \partial_\gamma u_\delta$, and the fluctuating stress $\sigma_{\alpha\beta}^f$. The influence of the particles is described via an external force density \vec{f}^h .

The coupling to a particle i is introduced via an interpolation procedure where first the flow velocities from the surrounding sites are averaged over to yield the flow velocity right

at the position of i . In the continuum limit, this is written as

$$\vec{u}_i \equiv \vec{u}(\vec{r}_i) = \int d^3\vec{r} \Delta(\vec{r}, \vec{r}_i) \vec{u}(\vec{r}), \quad (8)$$

where $\Delta(\vec{r}, \vec{r}_i)$ is a weight function with compact support, satisfying

$$\int d^3\vec{r} \Delta(\vec{r}, \vec{r}_i) = 1. \quad (9)$$

Secondly, each particle is assigned a phenomenological friction coefficient Γ_i , and this allows us to calculate the friction force on particle i :

$$\vec{F}_i^d = -\Gamma_i \left(\frac{\vec{p}_i}{m_i} - \vec{u}_i \right). \quad (10)$$

A Langevin noise term \vec{F}_i^f is added to the particle equation of motion, in order to compensate the dissipative losses that come from \vec{F}_i^d . \vec{F}_i^f satisfies the standard fluctuation–dissipation relation

$$\langle F_{i\alpha}^f \rangle = 0, \quad (11)$$

$$\langle F_{i\alpha}^f(t) F_{j\beta}^f(t') \rangle = 2k_B T \Gamma_i \delta_{ij} \delta_{\alpha\beta} \delta(t - t'), \quad (12)$$

where T is the absolute temperature and k_B the Boltzmann constant. While the conservative forces \vec{F}_i^c conserve the total momentum of the particle system, as a result of Newton’s third law, the dissipative and fluctuating terms (\vec{F}_i^d and \vec{F}_i^f) do not. The associated momentum transfer must therefore have come from the fluid. The overall momentum must be conserved, however. This means that the force term entering the Navier–Stokes equation must just balance these forces. One easily sees that the choice

$$\vec{f}^h(\vec{r}) = - \sum_i \left(\vec{F}_i^d + \vec{F}_i^f \right) \Delta(\vec{r}, \vec{r}_i) \quad (13)$$

satisfies this criterion. It should be noted that we use the *same* weight function to interpolate the forces back onto the fluid; this is necessary to satisfy the fluctuation–dissipation theorem for the overall system, i. e. to simulate a well–defined constant–temperature ensemble. The detailed proof of the thermodynamic consistency of the procedure can be found in Ref. 1.

We still need to specify the remaining terms in the Navier–Stokes equation. The viscosity tensor $\eta_{\alpha\beta\gamma\delta}$ describes an isotropic Newtonian fluid:

$$\eta_{\alpha\beta\gamma\delta} = \eta \left(\delta_{\alpha\gamma} \delta_{\beta\delta} + \delta_{\alpha\delta} \delta_{\beta\gamma} - \frac{2}{3} \delta_{\alpha\beta} \delta_{\gamma\delta} \right) + \eta_v \delta_{\alpha\beta} \delta_{\gamma\delta}, \quad (14)$$

with shear and bulk viscosities η and η_v . This tensor also appears in the covariance matrix of the fluctuating (Langevin) stress $\sigma_{\alpha\beta}^f$:

$$\langle \sigma_{\alpha\beta}^f \rangle = 0, \quad (15)$$

$$\langle \sigma_{\alpha\beta}^f(\vec{r}, t) \sigma_{\gamma\delta}^f(\vec{r}', t') \rangle = 2k_B T \eta_{\alpha\beta\gamma\delta} \delta(\vec{r} - \vec{r}') \delta(t - t'). \quad (16)$$

Finally, the Euler stress

$$\pi_{\alpha\beta}^E = p\delta_{\alpha\beta} + \rho u_\alpha u_\beta \quad (17)$$

describes the equation of state of the fluid (p is the thermodynamic pressure), and convective momentum transport.

3 Low Mach Number Physics

At this point an important simplification can be made. The equation of state only matters for flow velocities u that are comparable with the speed of sound c_s , i. e. for which the Mach number

$$Ma = \frac{u}{c_s} \quad (18)$$

is large. In the low Mach number regime, the flow may be considered as effectively incompressible (although no incompressibility constraint is imposed in the algorithm). The Mach number should not be confused with the Reynolds number Re , which rather measures whether inertial effects are important. Now it turns out that essentially all soft-matter applications “live” in the low- Ma regime. Furthermore, large Ma is anyways inaccessible to the LB algorithm, since it provides only a finite set of lattice velocities — and these essentially determine the value of c_s . In other words, the LB algorithm simply cannot realistically represent flows whose velocity is not small compared to c_s . For this reason, the details of the equation of state do not matter, and therefore one chooses the system that is by far the easiest — the ideal gas. Here the equation of state for a system at temperature T may be written as

$$k_B T = m_p c_s^2. \quad (19)$$

In the D3Q19 model (the most popular standard LB model in three dimensions, using nineteen lattice velocities, see below) it turns out that the speed of sound is given by

$$c_s^2 = \frac{1}{3} \frac{b^2}{h^2}, \quad (20)$$

where b is the lattice spacing and h the time step. Therefore the Boltzmann number can also be written as

$$Bo = \left(\frac{m_p}{\rho b^3} \right)^{1/2} = \left(\frac{3k_B T h^2}{\rho b^5} \right)^{1/2}. \quad (21)$$

4 Lattice Boltzmann 1: Statistical Mechanics

The lattice Boltzmann algorithm starts from a regular grid with sites \vec{r} and lattice spacing b , plus a time step h . We then introduce a small set of velocities \vec{c}_i such that $\vec{c}_i h$ connects two nearby lattice sites on the grid. In the D3Q19 model, the lattice is simple cubic, and the nineteen velocities correspond to the six nearest and twelve next-nearest neighbors, plus a zero velocity. On each lattice site \vec{r} at time t , there are nineteen populations $n_i(\vec{r}, t)$.

Each population is interpreted as the mass density corresponding to velocity \vec{c}_i . The total mass and momentum density are therefore given by

$$\rho(\vec{r}, t) = \sum_i n_i(\vec{r}, t), \quad (22)$$

$$\vec{j}(\vec{r}, t) = \sum_i n_i(\vec{r}, t) \vec{c}_i, \quad (23)$$

such that the flow velocity is obtained via $\vec{u} = \vec{j}/\rho$. The number of “lattice Boltzmann particles” which correspond to n_i is given by

$$\nu_i = \frac{n_i b^3}{m_p} \equiv \frac{n_i}{\mu}, \quad (24)$$

where m_p is the mass of a lattice Boltzmann particle, and μ the corresponding mass density. It should be noted that μ is a measure of the thermal fluctuations in the system, since, according to Eq. 21, one has $Bo^2 = \mu/\rho$.

If we now assume a “velocity bin” i to be in thermal contact with a large reservoir of particles, the probability density for ν_i is Poissonian. Furthermore, if we assume that the “velocity bins” are statistically independent, but take into account that mass and momentum density are fixed (these variables are conserved quantities during an LB collision step and should therefore be handled like conserved quantities in a microcanonical ensemble), we find

$$P(\{\nu_i\}) \propto \left(\prod_i \frac{\bar{\nu}_i^{\nu_i}}{\nu_i!} e^{-\bar{\nu}_i} \right) \delta \left(\mu \sum_i \nu_i - \rho \right) \delta \left(\mu \sum_i \nu_i \vec{c}_i - \vec{j} \right). \quad (25)$$

for the probability density of the variables ν_i . This must be viewed as the statistics which describes the local (single-site) equilibrium under the condition of fixed values of the hydrodynamic variables ρ and \vec{j} . The parameter $\bar{\nu}_i$ is the mean occupation imposed by the reservoir, and we assume that it is given by

$$\bar{\nu}_i = a^{c_i} \frac{\rho}{\mu}, \quad (26)$$

where $a^{c_i} > 0$ is a weight factor corresponding to the neighbor shell with speed c_i .

From normalization and cubic symmetry we know that the low-order velocity moments of the weights must have the form

$$\sum_i a^{c_i} = 1, \quad (27)$$

$$\sum_i a^{c_i} c_{i\alpha} = 0, \quad (28)$$

$$\sum_i a^{c_i} c_{i\alpha} c_{i\beta} = \sigma_2 \delta_{\alpha\beta}, \quad (29)$$

$$\sum_i a^{c_i} c_{i\alpha} c_{i\beta} c_{i\gamma} = 0, \quad (30)$$

$$\sum_i a^{c_i} c_{i\alpha} c_{i\beta} c_{i\gamma} c_{i\delta} = \kappa_4 \delta_{\alpha\beta\gamma\delta} + \sigma_4 (\delta_{\alpha\beta} \delta_{\gamma\delta} + \delta_{\alpha\gamma} \delta_{\beta\delta} + \delta_{\alpha\delta} \delta_{\beta\gamma}), \quad (31)$$

where σ_2 , σ_4 , κ_4 are yet undetermined constants, while $\delta_{\alpha\beta\gamma\delta}$ is unity if all four indexes are the same and zero otherwise.

Employing Stirling's formula for the factorial, it is straightforward to find the set of populations n_i^{eq} which maximizes P under the constraints of given ρ and \vec{j} . Up to second order in u (low Mach number!) the solution is given by

$$n_i^{eq} = \rho a^{c_i} \left(1 + \frac{\vec{u} \cdot \vec{c}_i}{\sigma_2} + \frac{(\vec{u} \cdot \vec{c}_i)^2}{2\sigma_2^2} - \frac{u^2}{2\sigma_2} \right). \quad (32)$$

The low-order moments of the equilibrium populations are then given by

$$\sum_i n_i^{eq} = \rho, \quad (33)$$

$$\sum_i n_i^{eq} c_{i\alpha} = j_\alpha, \quad (34)$$

$$\sum_i n_i^{eq} c_{i\alpha} c_{i\beta} = \rho c_s^2 \delta_{\alpha\beta} + \rho u_\alpha u_\beta. \quad (35)$$

The first two equations are just the imposed constraints, while the last one (meaning that the second moment is just the hydrodynamic Euler stress) follows from imposing two additional conditions, which is to choose the weights a^{c_i} such that they satisfy $\kappa_4 = 0$ and $\sigma_4 = \sigma_2^2$. From the Chapman–Enskog analysis of the LB dynamics (see below) it follows that the asymptotic behavior in the limit of large length and time scales is compatible with the Navier–Stokes equation only if Eq. 35 holds, and this in turn is only possible if the abovementioned isotropy conditions are satisfied. Together with the normalization condition, we thus obtain a set of three equations for the a^{c_i} . Therefore at least three neighbor shells are needed to satisfy these conditions, and this is the reason for choosing a nineteen-velocity model. For D3Q19, one thus obtains $a^{c_i} = 1/3$ for the zero velocity, $1/18$ for the nearest neighbors, and $1/36$ for the next-nearest neighbors. Furthermore, one finds $c_s^2 = \sigma_2 = (1/3)b^2/h^2$.

For the fluctuations around the most probable populations n_i^{eq} ,

$$n_i^{neq} = n_i - n_i^{eq}, \quad (36)$$

we employ a saddle-point approximation and approximate u by zero. This yields

$$P(\{n_i^{neq}\}) \propto \exp \left(- \sum_i \frac{(n_i^{neq})^2}{2\mu\rho a^{c_i}} \right) \delta \left(\sum_i n_i^{neq} \right) \delta \left(\sum_i \vec{c}_i n_i^{neq} \right). \quad (37)$$

We now introduce normalized fluctuations via

$$\hat{n}_i^{neq} = \frac{n_i^{neq}}{\sqrt{\mu\rho a^{c_i}}} \quad (38)$$

and transform to normalized “modes” (symmetry-adapted linear combinations of the n_i , see Ref. 1) \hat{m}_k^{neq} via an orthonormal transformation \hat{e}_{ki} :

$$\hat{m}_k^{neq} = \sum_i \hat{e}_{ki} \hat{n}_i^{neq}, \quad (39)$$

$k = 0, \dots, 18$, and obtain

$$P(\{m_k\}) \propto \exp\left(-\frac{1}{2} \sum_{k \geq 4} m_k^2\right). \quad (40)$$

It should be noted that the modes number zero to three have been excluded; they are just the conserved mass and momentum densities.

5 Lattice Boltzmann 2: Stochastic Collisions

A collision step consists of re-arranging the set of n_i on a given lattice site such that both mass and momentum are conserved. Since the algorithm should simulate thermal fluctuations, this should be done in a way that is (i) stochastic and (ii) consistent with the developed statistical-mechanical model. This is straightforwardly imposed by requiring that the collision is nothing but a Monte Carlo procedure, where a Monte Carlo step transforms the pre-collisional set of populations, n_i , to the post-collisional one, n_i^* . Consistency with statistical mechanics can be achieved by requiring that the Monte Carlo update satisfies the condition of detailed balance. Most easily this is done in terms of the normalized modes \hat{m}_k , which we update according to the rule ($k \geq 4$)

$$\hat{m}_k^* = \gamma_k \hat{m}_k + \sqrt{1 - \gamma_k^2} r_k. \quad (41)$$

Here the γ_k are relaxation parameters with $-1 < \gamma_k < 1$, and the r_k are statistically independent Gaussian random numbers with zero mean and unit variance. Mass and momentum are automatically conserved since the corresponding modes are not updated. Comparison with Eq. 40 shows that the procedure indeed does satisfy detailed balance. The parameters γ_k can in principle be chosen at will; however, they should be compatible with symmetry. For example, mode number four corresponds to the bulk stress, with a relaxation parameter γ_b , while modes number five to nine correspond to the five shear stresses, which form a symmetry multiplet. Therefore one must choose $\gamma_5 = \dots = \gamma_9 = \gamma_s$. For the remaining kinetic modes one often uses $\gamma_k = 0$ for simplicity, but this is not necessary.

6 Lattice Boltzmann 3: Chapman-Enskog Expansion

The actual LB algorithm now consists of alternating collision and streaming steps, as summarized in the LB equation (LBE):

$$n_i(\vec{r} + \vec{c}_i h, t + h) = n_i^*(\vec{r}, t) = n_i(\vec{r}, t) + \Delta_i \{n_i(\vec{r}, t)\}. \quad (42)$$

The populations are first re-arranged on the lattice site; this is described by the so-called “collision operator” Δ_i . The resulting post-collisional populations n_i^* are then propagated to the neighboring sites, as expressed by the left hand side of the equation. After that, the next collision step is done, etc.. The collision step may include momentum transfer as a result of external forces (for details, see Ref. 1); apart from that, it is just given by the update procedure outlined in the previous section.

A convenient way to find the dynamic behavior of the algorithm on large length and time scales is a multi-time-scale analysis. One introduces a “coarse grained ruler” by transforming from the original coordinates \vec{r} to new coordinates \vec{r}_1 via

$$\vec{r}_1 = \epsilon \vec{r}, \quad (43)$$

where ϵ is a dimensionless parameter with $0 < \epsilon \ll 1$. The rationale behind this is the fact that any “reasonable” value for the scale r_1 will automatically force r to be large. In other words: By considering the limit $\epsilon \rightarrow 0$ we automatically focus our attention on large length scales. The same is done for the time; however, here we introduce *two* scales via

$$t_1 = \epsilon t \quad (44)$$

and

$$t_2 = \epsilon^2 t. \quad (45)$$

The reason for this is that one needs to consider both wave-like phenomena, which happen on the t_1 time scale (i. e. the real time is moderately large), and diffusive processes (where the real time is *very* large). We now write the LB variables as a function of \vec{r}_1, t_1, t_2 instead of \vec{r}, t . Since changing ϵ at fixed \vec{r}_1 changes \vec{r} and thus n_i , we must take into account that the LB variables depend on ϵ :

$$n_i = n_i^{(0)} + \epsilon n_i^{(1)} + \epsilon^2 n_i^{(2)} + O(\epsilon^3). \quad (46)$$

The same is true for the collision operator:

$$\Delta_i = \Delta_i^{(0)} + \epsilon \Delta_i^{(1)} + \epsilon^2 \Delta_i^{(2)} + O(\epsilon^3). \quad (47)$$

In terms of the new variables, the LBE is written as

$$n_i(\vec{r}_1 + \epsilon \vec{c}_i h, t_1 + \epsilon h, t_2 + \epsilon^2 h) - n_i(\vec{r}_1, t_1, t_2) = \Delta_i. \quad (48)$$

Now, one systematically Taylor-expands the equation up to order ϵ^2 . Sorting by order yields a hierarchy of LBEs of which one takes the zeroth, first, and second velocity moment. Systematic analysis of this set of moment equations (for details, see Ref. 1) shows that the LB procedure, as it has been developed in the previous sections, indeed yields the fluctuating Navier–Stokes equations in the asymptotic $\epsilon \rightarrow 0$ limit — however only for low Mach numbers; in the high Mach number regime, where terms of order u^3/c_s^3 can no longer be neglected, the dynamics definitely deviates from Navier–Stokes.

In particular, this analysis shows that the zeroth-order populations must be identified with n_i^{eq} , and that it is *necessary* that this “encodes” the Euler stress via suitably chosen weights a^{c_i} . Furthermore, one finds explicit expressions for the viscosities:

$$\eta = \frac{h \rho c_s^2}{2} \frac{1 + \gamma_s}{1 - \gamma_s}, \quad (49)$$

$$\eta_b = \frac{h \rho c_s^2}{3} \frac{1 + \gamma_b}{1 - \gamma_b}. \quad (50)$$

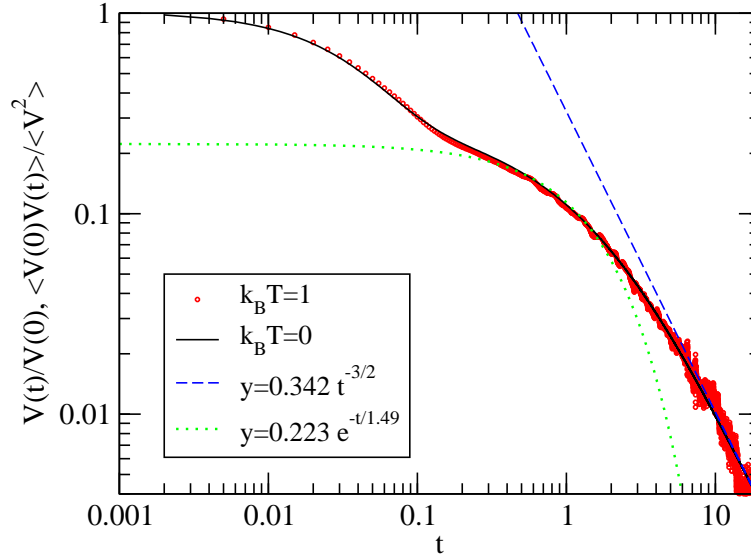


Figure 1. (From Ref. 5) Velocity autocorrelation function of a single colloidal sphere, normalized by the initial value, in thermal equilibrium. The velocity is here defined as the center-of-mass velocity of the particles which form the sphere. $\langle v^2 \rangle$, i. e. the $t = 0$ value of the unnormalized function, is therefore given by the equipartition theorem of statistical mechanics. For larger times, the surface particles become more and more coupled to the fluid inside the sphere, and thus the effective mass of the sphere increases. This is the reason for the first initial decay before a plateau is reached. After that, the function decays according to the famous $t^{-3/2}$ long-time tail. Finally, the particle becomes coupled to the whole fluid in the whole simulation box and the behavior becomes dominated by this finite-size effect. For comparison, the figure also shows the decay of the colloid velocity in a *deterministic* computer experiment, where the noise amplitude for both the particle dynamics and the LB degrees of freedom has been set to zero, and the particle was “kicked” at $t = 0$. This function has been normalized by the initial value, too. According to linear response theory, both curves must coincide, which they do.

7 Example: Dynamics of Charged Colloids

The coupling scheme that has been described in this article is particularly useful for immersed particles with internal degrees of freedom, like flexible polymer chains, or membranes. It can also be applied to systems whose immersed particles are “hard” (for example, colloidal spheres), although the alternative approach by Ladd (see Ref. 1) that models the particles as rigid bodies interacting with the LB fluid via boundary conditions is probably slightly more efficient. Nevertheless, for reasons of easy program development it makes sense to use the same scheme for both flexible and rigid systems. In what follows, some results for a colloidal system shall be presented, in order to demonstrate that and how the method works.

In Ref. 5 we have developed the so-called “raspberry model” for a colloidal sphere. Since the model is intended for charged systems with explicit (salt and counter) ions, it should take into account (at least to some degree) the size difference between colloids and ions. Therefore the colloid is, in terms of linear dimension, roughly 6–7 times larger than the small particles. The LB lattice spacing is chosen as identical to the small ion diameter. This is combined with a linear force interpolation to the nearest neighbor sites.

A larger lattice spacing would result in a rather coarse description of the hydrodynamic interactions, while a yet smaller spacing would result in a large computational overhead. In this context, it should be noted that one would obtain an ill-defined model with infinite particle mobility if one would let the lattice spacing tend to zero, while sticking to the nearest-neighbor interpolation scheme¹. This is due to the fact that the effective long-time mobility that results from the dissipative coupling is not given by $1/\Gamma$, but rather by

$$\frac{1}{\Gamma_{eff}} = \frac{1}{\Gamma} + \frac{1}{g\eta\sigma}, \quad (51)$$

where σ is the range of the interpolation function and g a numerical prefactor. Therefore, one needs to keep the range of the interpolation function constant, which would involve more and more effort if one would insist on $b \rightarrow 0$. Within limits, it is of course possible to compensate the effects of a change of σ by suitably re-adjusting Γ — only the long-time value Γ_{eff} is of real physical significance.

In principle, it would therefore be possible to model a colloidal sphere by a particle which exhibits a suitably chosen excluded-volume interaction for the other (small or large) particles, plus a suitably adjusted large value of the interpolation range σ , which essentially plays the role of a Stokes radius. However, such a model would not describe the rotational degrees of freedom, and these are important. For this reason, we rather model the colloid as a large sphere, around which we wrap a two-dimensional network of small particles (same size as the ions) which are connected via springs. Only the surface particles are coupled dissipatively to the LB fluid. Figures 1 and 2 show that the model behaves exactly as one would expect from hydrodynamics and linear response theory. Figure 1 shows the particle velocity autocorrelation function, from which one obtains, via integration, the translational (or self) diffusion coefficient D^S :

$$D^S = \frac{1}{3} \int_0^\infty dt \langle \vec{v}(t) \cdot \vec{v}(0) \rangle. \quad (52)$$

In an infinite hydrodynamic continuum, Stokes' law results in the prediction $D^S = k_B T / (6\pi\eta R)$ for a sphere of radius R . Indeed, this is what one finds in that limit. However, for (cubic) simulation boxes of finite linear dimension L , the diffusion constant is systematically smaller, as a result of the hydrodynamic interactions with the periodic images:

$$D^S = \frac{k_B T}{6\pi\eta R} - 2.837 \frac{k_B T}{6\pi\eta L}. \quad (53)$$

This is an analytic result, where higher-order terms in the L^{-1} expansion have been neglected. Figure 2 shows that this prediction is nicely reproduced. Furthermore, the rotational diffusion constant, which can be obtained by integrating the angular-velocity autocorrelation function,

$$D^R = \frac{1}{3} \int_0^\infty dt \langle \vec{\omega}(t) \cdot \vec{\omega}(0) \rangle, \quad (54)$$

exhibits a similar $1/L$ finite size effect; the asymptotic value $k_B T / (8\pi\eta R^3)$ is only reached for infinite system size. As Figure 2 shows, this prediction is reproduced as well.

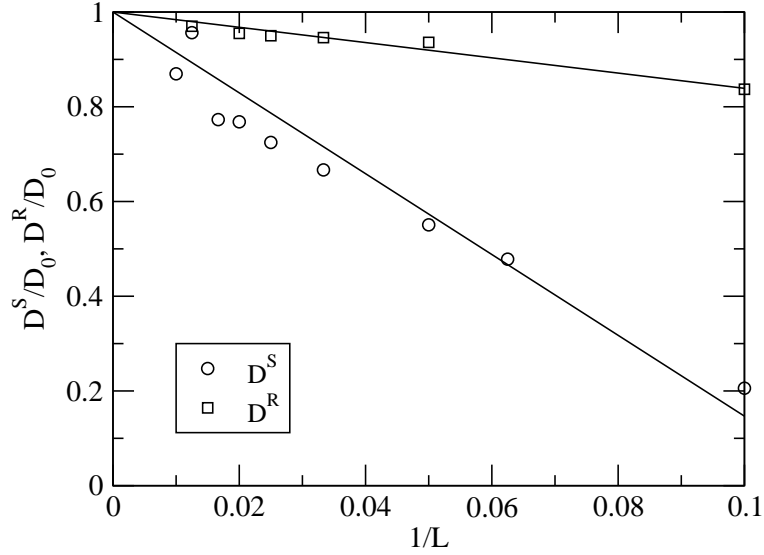


Figure 2. (From Ref. 5) Translational (D^S) and rotational (D^R) diffusion coefficient, normalized by the asymptotic infinite-system value, as a function of inverse system size $1/L$. The straight line is a fit for D^R , while it is the analytical prediction (see text) for D^S .

Electrokinetic phenomena can be investigated by supplying a charge to the central colloidal sphere, and by adding ions such that the total system is charge-neutral. We have studied the electrophoretic mobility, i. e. the response to an external electric field E :

$$\mu = \frac{v}{eE}, \quad (55)$$

where v is the colloid drift velocity and e the elementary charge. The simplest case is to simulate just a single colloid with charge Ze in a cubic box, and to add Z monovalent counterions to compensate the colloidal charge (i. e. no further salt ions are added). This corresponds to a system with a finite volume fraction (one colloid per box). It should be noted that one should *not* consider the limit where this system is being put into larger and larger boxes: In that case, the ions would simply “evaporate”, and one would obtain a trivial value for μ that is just given by Stokes’ law.

Usually the mobility is given in dimensionless units: The so-called reduced mobility μ_{red} is obtained by normalizing with a Stokes mobility, using the Bjerrum length l_B as the underlying length scale:

$$\mu_{red} = 6\pi\eta l_B \mu, \quad (56)$$

$$l_B = \frac{e^2}{4\pi\epsilon k_B T}, \quad (57)$$

where ϵ is the fluid’s dielectric constant.

Fortunately, μ is subject to a much smaller finite size effect than the diffusion constant. This has been checked by simulations, see Fig. 3. The reason for this behavior is the fact that the electric field does not exert a net force on the overall system, due to charge

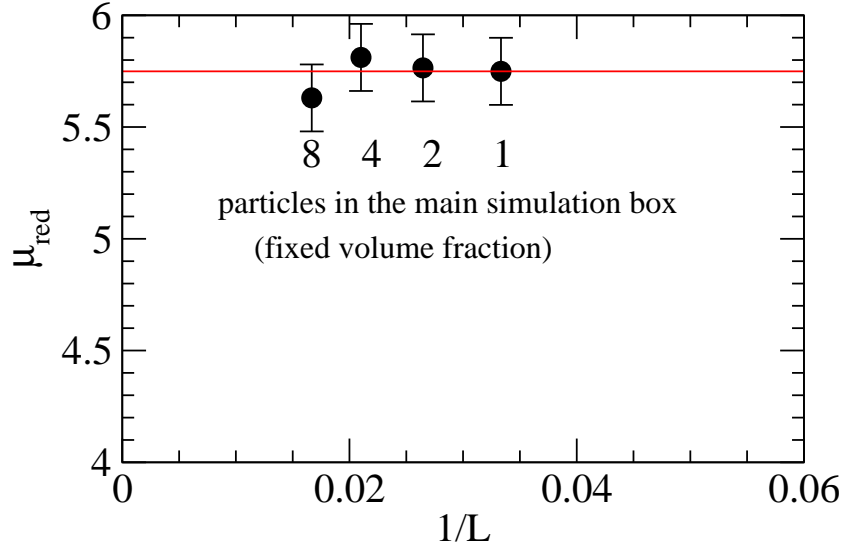


Figure 3. Reduced electrophoretic mobility as a function of inverse system size $1/L$. In order to keep conditions constant (i. e. constant colloidal volume fraction, and constant ion concentration), the box size was systematically increased, while at the same time more and more colloids (up to eight), together with their compensating ions, were put into the box. Within our resolution, no finite size effect could be detected.

neutrality. In other words: The field induces two electric currents in opposite direction. These currents, in turn, induce hydrodynamic flows. These flows, however, cancel each other exactly in leading order. Therefore the hydrodynamic interactions with the periodic images are weak. This should be contrasted with the diffusion constant, which corresponds to the response to an external gravitational field. The latter *does* exert a net force on the overall system, and hence one obtains a large-scale flow decaying like the inverse distance from the colloid. This $1/r$ flow field is exactly the reason for the $1/L$ finite-size effect in the diffusion constant as shown in Fig. 2.

The electrophoretic mobility may be obtained by either applying an electric field, and measuring the drift velocity, or by Green-Kubo integration⁶, where a system in strict thermal equilibrium is studied:

$$k_B T \mu = \frac{1}{3} \sum_i z_i \int_0^\infty dt \langle \vec{v}_i(0) \cdot \vec{v}_0(t) \rangle, \quad (58)$$

where the index i denotes particle number i , and z_i is its valence. Particle number zero is the colloid whose response to the electric field is considered. The nonequilibrium approach is hampered by the fact that, for reasonable electric field values, the response is quite typically in the nonlinear regime (mainly as a result of charge-cloud stripping). Therefore, one needs to extrapolate to zero driving. In contrast, the Green-Kubo value is, *per definition*, the linear-response result. Figure 4 shows that the two approaches yield the same result.

Further results that have been obtained with this model include a study of the concentration dependence of μ , both in terms of colloid volume fraction of a salt-free system, and in terms of salt concentration at fixed colloid concentration. Without going into further de-

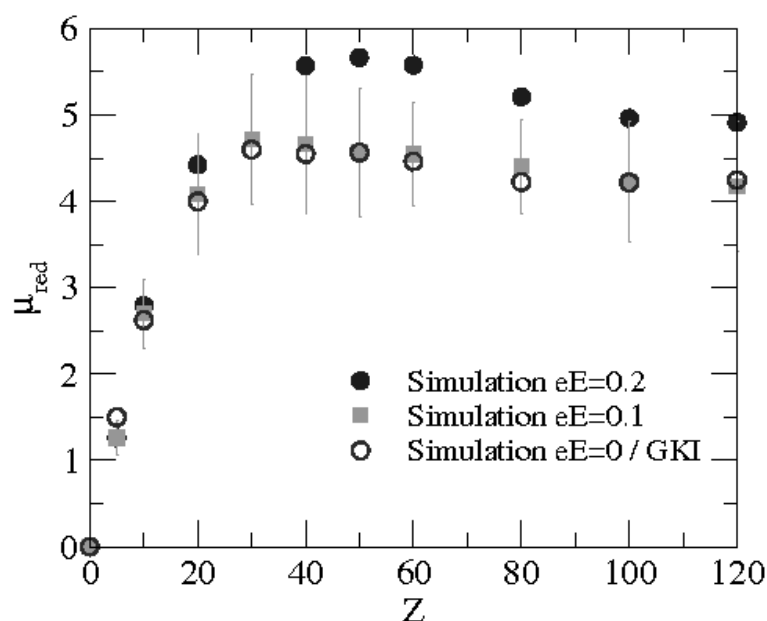


Figure 4. (From Ref. 6) Reduced electrophoretic mobility for the single-colloid system described in the text, as a function of the colloid's charge Z , comparing nonequilibrium with Green-Kubo integration (GKI) results. The mobility first increases, since the force is proportional to the charge. However, for larger Z values it saturates, indicating that more and more ions condense at the colloid's surface, such that the effective charge does not change. For $eE = 0.2$, nonlinear effects lead to an increased mobility, while $eE = 0.1$ is still in the linear-response regime, as demonstrated by the comparison with the equilibrium data.

tails, it should just be mentioned that the reduced-mobility data can be nicely rationalized in terms of a scaling theory⁶ which then allows a favorable comparison with experimental results⁷.

Of course, this is not the only example where the coupled MD-LB approach has helped to understand the dynamics of soft matter. Other examples include the dynamics of polymers and neutral colloids in both equilibrium and nonequilibrium situations; these have been outlined in Ref. 1. Further simulations will follow in the future, and it seems that the method is gaining popularity in the soft-matter community.

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